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STUDIES ON THE RECLAMATION OF WASTE RUBBER FROM LATEX BASED RUBBER INDUSTRIES

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### INTRODUCTION

In India, the total consumption of rubber by latex based rubber industries comes to about 20,000 M. Tonnes. The waste rubber formed in latex based rubber industries is around 10 to 15% of the rubber consumed. The formation of a higher percentage of waste rubber in latex factories (WLR) is due to the unstable nature of latex compound and the strict specifications on the quality of latex products such as condoms and surgical gloves. These waste materials contain about 90 to 95% rubber hydrocarbon. So far no attempt has been reported to recover rubber from these polymer enriched WLR. Considerable work has been done on the reclamation of scrap rubber from dry rubber products by chemical<sup>1</sup>, thermochemical<sup>3</sup>, and cryomechanical<sup>5</sup>, 7 processes.

In the present study, it is proposed to develop a process for reclaiming WLR. The effect of incorporation of reclaimed WLR on the properties of tread compound is also studied.

#### EXPERIMENTAL

Waste condom supplied by M/s Hindustan Latex Ltd. was used as the starting material for the study. The reclaiming agent used was activated pentachlorothiophenol (Renacit-7) procured from M/s Bayer India Ltd.

Standardisation of the reclaiming process

The waste rubber was powdered by passing through a hot two roll mill (80-90°C) to a size of about 40

mesh. The powdered material was admixed with 10 parts by weight of naphthenic oil and different dosages of reclaiming agent in a cold mill. The resulting compound was heated in an air oven at different temperatures (80-140°C) for different periods of time. The extent of degradation was assessed by measuring the Wallace plasticity (Po) of the treated material. The results are given in Table-1.

# Characterisation of reclaimed WLR

Characteristics like volatile matter, ash content, acetone extract and rubber hydrocarbon of the reclaimed WLR were determined as per IS 6306-1971. Results are given in Table-2. For comparison, the values for the above parameters for Whole Tyre Reclaim (WTR) were determined and are given in the same table.

The processing and technological properties of compound containing reclaimed WLR were evaluated in comparison with compound containing equivalent loadings of WTR. For this 3 tread compounds were prepared as per formula given in Table-3. The properties of these compounds were evaluated as per relevant IS/ASTM test methods. The test results are given in Table-4. Based on the laboratory evaluation, 3 tread compounds as described earlier were prepared again and these were used for retreading car tyres for assessing the service performance.

## RESULTS AND DISCUSSION

The effect of dosage of activated pentachlorothiophenol, temperature and time of heating on the extent
of degradation as indicated by plasticity, are shown
in Table-1. Results show that the extent of degradation increases with increase in the dosage of reclaiming agent, temperature and time of heating. The reclaimed material is found to form a smooth band on
the mill when the Po value is in the range of 25 to
30. So in this study, the conditions which resulted
in reclaimed rubbers having plasticity in the range
25 to 30, were selected as the optimum conditions for
reclaiming. From the results in Table-1, it is seen
that the following conditions are suitable for
reclaiming WLR.

- (i) Reclaiming agent 1% and heating at 140°C for 30 minutes
- (ii) Reclaiming agent 0.25% and heating at 140°C for 60 minutes

In the present studies, the first set of conditions

The composition of reclaimed WLR as shown in Table-2 reveals that it contains 82% rubber hydrocarbon whereas the WTR contains only 48% rubber hydrocarbon. It is observed from physical properties of vulcanizates (Table-4) that addition of reclaimed rubber causes a decrease in tensile strength, elongation, resilience, tear strength, flex resistance and abrasion resistance. Compression set is not much affected by the addition of reclaimed WLR. increase in heat build up and hardness is also observed. But the compound containing reclaimed WLR shows better processing characteristics and physical properties when compared with that containing WTR. The same trend is also observed from the service performance of the retreads (Table-5). The tread prepared with the incorporation of reclaimed WLR gave higher mileage than the one prepared with equivalent amount of WTR.

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Table 1. Effect of dosage of reclaiming agent. temperature and time of heating on plasticity

| 4             | 1.0                  | 80          | 61             | . 50                                    |  |  |
|---------------|----------------------|-------------|----------------|---|--|--|
| 3             | 0.5                  | 80          |                |   |  |  |
| 2             |                      |             | 60             | 55                                      |  |  |
| 2             | 0.25                 | 80          | 61             | 57                                      |  |  |
| 1             | . 0                  | 80          | 98             | 98                                      |  |  |
| TEE:          | (                    | (3)         | \              | , |  |  |
| (1)           | (2)                  | (3)         | (4)            | (5)                                     |  |  |
| ===           | ******               | ZZZZ===     |                |   |  |  |
| No.           | reclaiming agent (%) | rature (°C) | 30 minutes Po  | 60 minutes Po                           |  |  |
| S1. Dosage of |                      | Tempe-      |                | Heating time                            |  |  |
| ***           |                      | *******     | 3=332XXXXXXXXX | XX = X = X = X X X X X X X X X X X X X  |  |  |

(Table 1 contd...)

| ====== | ******** | ********* | ======== | *****      |
|--------|----------|-----------|----------|------------|
| (1)    | (2)      | (3)       | (4)      | (5)        |
| *===== | *****    |           | PETETEE  | **======== |
| 5      | . 0      | 100       | 96       | 94         |
| 6      | 0.25     | 100       | 57       | 58         |
| 7      | . 0.5    | 100       | 58       | 54         |
| 8      | 1.0      | 100       | 49       | 53         |
| 9      | - 0      | 120       | 96       | 90         |
| 10     | 0.25     | 120       | 66       | 60         |
| 11     | 0.5      | 120       | 60       | 58         |
| 12     | 1.0      | 120       | 53       | 57         |
| 13     | . 0      | 130       | 95       | 95         |
| 14     | 0.25     | - : 130 - | 57       | 63         |
| 15     | 0.50     | 130       | 58       | 55         |
| 16     | 1.0.     | 130       | 49       | 45         |
| 17     | 0        | 140       | 80       | 64         |
| 18     | 0.25     | 140       | 44       | 26         |
| 19     | 0.50     | 140       | 41       | 19         |
| 20     | 1.0      | 140       | 24       | 12         |
| ====== | ******** |           | ******** |            |

Table 2. Characterisation of reclaim.

| Parameters             | Reclaimed<br>WLR | Whole tyre reclaim (WTR) |
|------------------------|------------------|--------------------------|
| **********             | EMISESPHENSES:   | - HENEFERENEES           |
| Volatile matter (%)    | 0.01             | 0.60                     |
| Acetone extract (%)    | 15.54            | 12.97                    |
| Ash content (%)        | 2.40             | 7.93                     |
| Carbon black (%)       |                  | 30.49                    |
| Rubber hydrocarbon (%) | 82.05            | 48.01                    |

Table 3. Compounding recipe.

| Tuning! aut a                          |   | Parts | by we | eight |  |
|--|---|-------|-------|-------|--|
| Ingredients                            |   | I     | II    | III   |  |
| Natural rubber (RSS.1)                 |   | 100   | 80    | 80    |  |
| Reclaimed WLR                          |   | -     | 24.4  | -     |  |
| Whole tyre reclaim (W)                 | rr)                                     |       |       | 41.6  |  |
| Zinc oxide                             |   | 5     | 5     | 5     |  |
| Stearic acid                           | 424.1                                   | 2     | . 2   | 2     |  |
| Phenyl B-naphthylamine                 | • | 1     | 1     | . 1   |  |
| N-(1,3 dimethyl butyl)                 |   |       | an'   |       |  |
| phenyl p-phenylene                     | diamine                                 | 1     | 1     | 1     |  |
| HAF black (N 330)                      | 1.                                      | 50    | 50    | 50    |  |
| Aromatic oil                           |   | 5     | 5     | 5     |  |
| N-Cyclohexyl-2-benzoth<br>sulphenamide | niazyi                                  | 0.6   | 0.6   | 0.6   |  |
| Sulphur                                |   | 2.5   | 2.5   | 2.5   |  |

|     | Properties                             | I     | / II      | III   |
|-----|--|-------|-----------|-------|
| 1.  | Modulus at 300%                        |       |           | ===== |
|     | elongation (kg/cm <sup>2</sup> )       | 93 .  | 97        | 95    |
| 2.  | Tensile strength (kg/cm <sup>2</sup> ) | 273   | 233       | 198   |
| 3.  | Elongation at break (%)                | 660   | 604       | 540   |
| 4.  | After ageing at 70°C for 96 hours      |       |           |       |
|     | a) Retention of modulus at             |       |           |       |
|     | 300% elongation (%)                    | 129   | 123       | 127   |
|     | b) Retention of tensile                |       |           | 1     |
|     | strength (%)                           | 95    | 93        | :95   |
|     | c) Retention of elongation             |       |           |       |
|     | at break (%)                           | 85    | 81        | 81    |
| 5.  | Tear strength(kg/cm)                   | 106   | 86        | 79    |
| 6.  | Abrasion resistance (loss              |       |           |       |
|     | in volume, cc/hr)                      | 0.64  | 0.69      | 0.78  |
| 7.  | Hardness (Shore A)                     | 61    | 65        | 69    |
| 8.  | Heat build up at 50°C                  |       |           | 1.00  |
|     | (ΔT, °C)                               | 23    | 25        | 32    |
| 9.  | Compression set (%)                    | 34    | 34        | 40    |
| 10. | Rebound resilience (%)                 | 51    | 45        | 43    |
| 11. |  |       |           |       |
|     | Crack initiation                       | 71    | 42        | 31    |
|     | Crack failure                          | 229   | 179       | 94    |
|     | e time at 150°C (Ninutes)              | 10    | 9         | 9.5   |
| Sco | rch time at 120°C (Minutes)            | 25    | 17        | 14    |
| === |  | ===== |           | ===== |
| Tab | ole 5. Service performance of          | *     | ads.      |       |
| Com | pound Original Distance Pres           |       | Projected |       |
|     |  |       | mileage   |       |
|     | depth (km) dept                        |       | (km)      |       |
|     | (1/32") (1/3                           |       |           | 14-14 |
| === |  |       |           | ====  |
|     | I 12 3674 8.2                          | 25    | 11,756    |       |
|     | II 12 3674 7.7                         |       | 10,373    |       |
|     | II 12 3674 7.5                         |       | 9,797     |       |

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